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APPLICATION FOR LETTERS PATENT

Title : PLASMA DISPLAY DEVICE

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## CROSS-REFERENCE TO RELATED APPLICATIONS

This application is based upon and claims the benefit of priority from the prior Japanese Patent Application No. 2003-138546, filed on May 16, 2003, the entire contents of which are incorporated herein by reference.

## BACKGROUND OF THE INVENTION

### [Field of the Invention]

The present invention relates to a plasma display device.

### [Description of the Related Art]

Fig. 34 is a diagram showing the basic configuration of a plasma display device. A control circuit section 1101 controls an address driver 1102, a sustain electrode (X electrode) sustain (sustain discharge) circuit 1103, a scan electrode (Y electrode) sustain circuit 1104, and a scan driver 1105.

The address driver 1102 supplies a predetermined voltage to address electrodes A1, A2, A3, .... Hereafter, each of the address electrodes A1, A2, A3, ... or their generic name is an address electrode Aj, j representing a suffix.

The scan driver 1105 supplies a predetermined voltage to scan electrodes Y1, Y2, Y3, ... in accordance with control of the control circuit section 1101 and the scan electrode sustain circuit

1104. Hereafter, each of the scan electrodes  $Y_1$ ,  $Y_2$ ,  $Y_3$ , ... or their generic name is a scan electrode  $Y_i$ ,  $i$  representing a suffix.

The sustain electrode sustain circuit 1103 supplies the same voltage to sustain electrodes  $X_1$ ,  $X_2$ ,  $X_3$ , ... respectively. Hereafter, each of the sustain electrodes  $X_1$ ,  $X_2$ ,  $X_3$ , ... or their generic name is a sustain electrode  $X_i$ ,  $i$  representing a suffix. The sustain electrodes  $X_i$  are connected to each other and have the same voltage level.

Within a display region 1107, the scan electrodes  $Y_i$  and the sustain electrodes  $X_i$  form rows extending in parallel in the horizontal direction, and the address electrodes  $A_j$  form columns extending in the vertical direction. The scan electrodes  $Y_i$  and the sustain electrodes  $X_i$  are alternately arranged in the vertical direction. Ribs 1106 have a stripe rib structure provided between the address electrodes  $A_j$ .

The scan electrodes  $Y_i$  and the address electrodes  $A_j$  form a two-dimensional matrix with  $i$  rows and  $j$  columns. A display cell  $C_{ij}$  is formed of an intersection of the scan electrode  $Y_i$  and the address electrode  $A_j$  and the sustain electrode  $X_i$  correspondingly adjacent thereto. This display cell  $C_{ij}$  corresponds to a pixel, so that the display region 1107 can display a two-dimensional image.

Fig. 35A is a view showing the configuration of a cross section of the display cell  $C_{ij}$  in Fig. 34.

The sustain electrode  $X_i$  and the scan electrode  $Y_i$  are formed on a front glass substrate 1211. A dielectric layer 1212 for insulating the electrodes from a discharge space 1217 is applied thereover, and a MgO (magnesium oxide) protective film 1213 is further applied over the dielectric layer 1212.

On the other hand, the address electrode  $A_j$  is formed on a rear glass substrate 1214 which is disposed to oppose the front glass substrate 1211, a dielectric layer 1215 is applied thereover, and further phosphors are applied over the dielectric layer 1215. In the discharge space 1217 between the MgO protective film 1213 and the dielectric layer 1215, a Ne+Xe Penning gas or the like is sealed.

Fig. 35B is a view for explaining a capacitance  $C_p$  of an AC drive type plasma display. A capacitance  $C_a$  is a capacitance of the discharge space 1217 between the sustain electrode  $X_i$  and the scan electrode  $Y_i$ . A capacitance  $C_b$  is a capacitance of the dielectric layer 1212 between the sustain electrode  $X_i$  and the scan electrode  $Y_i$ . A capacitance  $C_c$  is a capacitance of the front glass substrate 1211 between the sustain electrode  $X_i$  and the scan electrode  $Y_i$ . The sum of the capacitances  $C_a$ ,  $C_b$ , and  $C_c$  determines the capacitance between the electrodes  $X_i$  and  $Y_i$ .

Fig. 35C is a view for explaining light emission of the AC drive type plasma display. On an inner

surface of a rib 1216, phosphors 1218 in red, blue and green are applied, arranged in stripes for each color, so that a discharge between the sustain electrode  $X_i$  and the scan electrode  $Y_i$  excites the phosphors 1218 to generate light 1221.

Fig. 36 is a diagram of the configuration of one frame FR of an image. The image is formed of, for example, 60 frames per second. One frame FR is formed of a first subframe SF1, a second subframe SF2, ..., and an nth subframe SFn. This n is, for example, 10, and corresponds to the number of grayscale bits. Each of the subframes SF1, SF2, and so on or their generic name is a subframe SF hereafter.

Each subframe SF is composed of a reset period  $T_r$ , an address period  $T_a$ , and a sustain period (sustain discharge period)  $T_s$ . During the reset period  $T_r$ , the display cell is initialized. During the address period  $T_a$ , lighting or non-lighting of each display cell can be selected by addressing. The selected cell emits light during the sustain period  $T_s$ . The number of light emissions (period of time) is different in each SF. This can determine a grayscale value.

Fig. 37 shows a driving method during the sustain period  $T_s$  of a progressive method plasma display. At time  $t_1$ , an anode potential  $V_{s1}$  is applied to the sustain electrodes  $X_{n-1}$ ,  $X_n$ , and  $X_{n+1}$ , and a cathode

potential  $V_{s2}$  is applied to the scan electrodes  $Y_{n-1}$ ,  $Y_n$ , and  $Y_{n+1}$ . This applies a high voltage respectively between the sustain electrode  $X_{n-1}$  and the scan electrode  $Y_{n-1}$ , between the sustain electrode  $X_n$  and the scan electrode  $Y_n$ , and between the sustain electrode  $X_{n+1}$  and the scan electrode  $Y_{n+1}$  to perform sustain discharges 1410.

Subsequently, at time  $t_2$ , the cathode potential  $V_{s2}$  is applied to the sustain electrodes  $X_{n-1}$ ,  $X_n$ , and  $X_{n+1}$ , and the anode potential  $V_{s1}$  is applied to the scan electrodes  $Y_{n-1}$ ,  $Y_n$ , and  $Y_{n+1}$ . This applies a high voltage respectively between the sustain electrode  $X_{n-1}$  and the scan electrode  $Y_{n-1}$ , between the sustain electrode  $X_n$  and the scan electrode  $Y_n$ , and between the sustain electrode  $X_{n+1}$  and the scan electrode  $Y_{n+1}$  to perform sustain discharges 1410.

Subsequently, at time  $t_3$ , the same potentials as those at time  $t_1$  are applied to perform sustain discharges 1410, and at time  $t_4$ , the same potentials as those at time  $t_2$  are applied to perform sustain discharges 1410.

Fig. 38 shows a driving method during the sustain period  $T_s$  of a plasma display by an ALIS (Alternate Lighting of Surfaces) method. At time  $t_1$ , the anode potential  $V_{s1}$  is applied to the sustain electrodes  $X_{n-1}$  and  $X_{n+1}$  on odd-numbered rows, and the cathode potential  $V_{s2}$  is applied to the scan electrodes  $Y_{n-1}$  and  $Y_{n+1}$  on odd-numbered rows. Further, the cathode

potential  $V_{s2}$  is applied to the sustain electrode  $X_n$  on an even-numbered row, and the anode potential  $V_{s1}$  is applied to the scan electrode  $Y_n$  on an even-numbered row. This applies a high voltage respectively between the sustain electrode  $X_{n-1}$  and the scan electrode  $Y_{n-1}$ , between the sustain electrode  $X_n$  and the scan electrode  $Y_n$ , and between the sustain electrode  $X_{n+1}$  and the scan electrode  $Y_{n+1}$  to perform sustain discharges 1510.

Subsequently, at time  $t_2$ , the cathode potential  $V_{s2}$  is applied to the sustain electrodes  $X_{n-1}$  and  $X_{n+1}$  on the odd-numbered rows, and the anode potential  $V_{s1}$  is applied to the scan electrodes  $Y_{n-1}$  and  $Y_{n+1}$  on the odd-numbered rows. Further, the anode potential  $V_{s1}$  is applied to the sustain electrode  $X_n$  on the even-numbered row, and the cathode potential  $V_{s2}$  is applied to the scan electrode  $Y_n$  on the even-numbered row. This applies a high voltage respectively between the sustain electrode  $X_{n-1}$  and the scan electrode  $Y_{n-1}$ , between the sustain electrode  $X_n$  and the scan electrode  $Y_n$ , and between the sustain electrode  $X_{n+1}$  and the scan electrode  $Y_{n+1}$  to perform sustain discharges 1510.

Subsequently, at time  $t_3$ , the same potentials as those at time  $t_1$  are applied to perform sustain discharges 1510, and at time  $t_4$ , the same potentials as those at time  $t_2$  are applied to perform sustain discharges 1510.

The above-described ALIS method is also described in the following patent document 1. Further, the following patent documents 2 and 3 are disclosed.

(Patent Document 1)

Japanese Patent No. 2801893 (USP 6373452)

(Patent Document 2)

Japanese Patent No. 3201603 (EP 01065650)

(Patent Document 3)

Japanese Patent Application Laid-open No. 2003-15585 (US 2003-0001801)

#### SUMMARY OF THE INVENTION

An object of the present invention is to provide a plasma display device having a high image quality display mode capable of performing a stable sustain discharge by reducing the influence of adjacent display cells, a low power display mode capable of performing a sustain discharge with a low power, and/or a high luminance display mode capable of performing a sustain discharge with high luminance.

According to one aspect of the present invention, a plasma display device is provided which includes a plurality of X electrodes, a plurality of Y electrodes arranged adjacent to the plurality of X electrodes for causing sustain discharges between the plurality of X electrodes and the plurality of Y electrodes, an X electrode drive circuit for applying a sustain discharge voltage to the plurality of X



electrodes, and a Y electrode drive circuit for applying a sustain discharge voltage to the plurality of Y electrodes. The X electrode drive circuit and the Y electrode drive circuit have a first sustain drive mode in which discharge pulses to predetermined adjacent electrodes rise or fall in the same direction at the same time and a second sustain drive mode in which discharge pulses to all adjacent electrodes rise or fall at different timings.

In the second sustain drive mode, it is possible to prevent changes on the X electrode and the Y electrode for performing a sustain discharge from diffusing to adjacent electrodes, thus making it possible to eliminate an error display and perform a high image quality display. In the first sustain drive mode, the plasma display device can perform a low lower display when driven with the same number of discharge pulses as that in the second sustain drive mode, and can perform a high luminance display when driven with the same power consumption as that in the second sustain drive mode because the number of sustain discharge pulses increases.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a diagram showing the configuration of a plasma display device according to a first embodiment of the present invention;

Fig. 2 is a timing chart showing sustain discharge pulses during a sustain period in a high image quality mode;

Fig. 3 is a timing chart showing sustain discharge pulses during a sustain period in a low power mode and a high luminance mode;

Fig. 4 is a diagram showing the configuration of a plasma display device according to a second embodiment of the present invention;

Fig. 5 is a diagram showing a configuration example of a power supply current detection circuit;

Fig. 6 is a timing chart showing voltage waveforms at a sustain electrode, a scan electrode, and an address electrode in the high image quality mode and the low power mode;

Fig. 7 is a timing chart showing voltage waveforms at the sustain electrode, the scan electrode, and the address electrode in the high luminance mode;

Fig. 8 is a diagram showing the configuration of a plasma display device according to a third embodiment of the present invention;

Fig. 9 is a diagram showing the configuration of a plasma display device according to a fourth embodiment of the present invention;

Fig. 10 is a diagram showing the configuration of a plasma display device according to a fifth embodiment of the present invention;

Fig. 11 is a cross-sectional view of a progressive method plasma display;

Fig. 12 is a timing chart showing a driving method during a sustain period of a progressive method plasma display according to a sixth embodiment of the present invention;

Figs. 13A to 13C are diagrams showing applied voltages to electrodes during a first discharge;

Figs. 14A to 14C are diagrams showing applied voltages to electrodes during a second discharge;

Figs. 15A to 15C are diagrams showing applied voltages to electrodes during a third discharge;

Figs. 16A to 16C are diagrams showing applied voltages to electrodes during a fourth discharge;

Fig. 17 is a timing chart showing a driving method during a sustain period of a progressive method plasma display according to a seventh embodiment of the present invention;

Fig. 18 is a timing chart showing a driving method during a sustain period of a progressive method plasma display according to an eighth embodiment of the present invention;

Figs. 19A to 19C are diagrams showing a problem of applied voltages to electrodes during a first discharge in Fig. 18;

Figs. 20A to 20C are diagrams showing applied voltages to the electrodes during the first discharge in Fig. 18;

Fig. 21 is a timing chart showing a driving method during a sustain period of a progressive method plasma display according to a ninth embodiment of the present invention;

Fig. 22 is a timing chart showing a driving method during a sustain period of a progressive method plasma display according to a tenth embodiment of the present invention;

Fig. 23 is a timing chart showing a driving method during a sustain period of a progressive method plasma display according to an eleventh embodiment of the present invention;

Fig. 24 is a diagram showing an arrangement of electrodes of a progressive method plasma display according to a twelfth embodiment of the present invention;

Fig. 25 is a cross-sectional view of an ALIS method plasma display according to a thirteenth embodiment of the present invention;

Figs. 26A and 26B are timing charts each showing a driving method during a sustain period of an ALIS method plasma display according to the thirteenth embodiment;

Figs. 27A and 27B are timing charts each showing a driving method during a sustain period of an ALIS method plasma display according to a fourteenth embodiment of the present invention;

Figs. 28A and 28B are timing charts each showing a driving method during a sustain period of an ALIS method plasma display according to a fifteenth embodiment of the present invention;

Figs. 29A and 29B are timing charts each showing a driving method during a sustain period of an ALIS method plasma display according to a sixteenth embodiment of the present invention;

Figs. 30A and 30B are timing charts each showing a driving method during a sustain period of an ALIS method plasma display according to a seventeenth embodiment of the present invention;

Figs. 31A and 31B are timing charts each showing a driving method during a sustain period of an ALIS method plasma display according to an eighteenth embodiment of the present invention;

Figs. 32A and 32B are circuit diagrams of sustain electrode sustain circuits and scan electrode sustain circuits according to a nineteenth and a twentieth embodiment of the present invention;

Figs. 33A to 33C are diagrams showing voltage waveforms of sustain discharges;

Fig. 34 is a diagram showing the configuration of a plasma display device;

Figs. 35A to 35C are cross-sectional views of a display cell of a plasma display;

Fig. 36 is a diagram of the configuration of a frame of an image;

Fig. 37 is a diagram showing waveforms during a sustain period of a progressive method plasma display; and

Fig. 38 is a diagram showing waveforms during a sustain period of an ALIS method plasma display.

#### DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

With an increase in definition of plasma displays, the distance between adjacent electrodes decreases. This results in shortened distances from the sustain electrode  $X_n$  and the scan electrode  $Y_n$  constituting the discharge space to the scan electrode  $Y_{n-1}$  and the sustain electrode  $X_{n+1}$  arranged adjacent thereto, respectively.

Therefore, when a discharge is caused between the sustain electrode  $X_n$  and the scan electrode  $Y_n$ , electrons on the scan electrode  $Y_{n-1}$  or the sustain electrode  $X_{n+1}$  are likely to diffuse (transfer) to cause an adjacent display cell constituted of the sustain electrode  $X_{n-1}$  and the scan electrode  $Y_{n-1}$  or the sustain electrode  $X_{n+1}$  and the scan electrode  $Y_{n+1}$  to perform error display such that the display cell lights up during time when the display cell should turn off, or the display cell turns off during time when the display cell should light up because the electrodes cannot sustain a discharge.

-First Embodiment-

Fig. 1 is a diagram showing the configuration of a plasma display device according to a first embodiment of the present invention. A control circuit section 101 controls an address driver 102, sustain electrode (X electrode) sustain circuits 103a and 103b, scan electrode (Y electrode) sustain circuits 104a and 104b, and scan drivers 105a and 105b.

The address driver 102 supplies a predetermined voltage to address electrodes A1, A2, A3, .... Hereafter, each of the address electrodes A1, A2, A3, ... or their generic name is an address electrode Aj, j representing a suffix.

The first scan driver 105a supplies a predetermined voltage to scan electrodes (first discharge electrodes) Y1, Y3, ... on odd-numbered rows in accordance with control of the control circuit section 101 and the first scan electrode sustain circuit 104a. The second scan driver 105b supplies a predetermined voltage to scan electrodes Y2, Y4, ... on even-numbered rows in accordance with control of the control circuit section 101 and the second scan electrode sustain circuit 104b. Hereafter, each of the scan electrodes Y1, Y2, Y3, ... or their generic name is a scan electrode Yi, i representing a suffix.

The first sustain electrode sustain circuit 103a supplies the same voltage to sustain electrodes

(second discharge electrodes)  $X_1, X_3, \dots$  on odd-numbered rows, respectively. The second sustain electrode sustain circuit 103b supplies the same voltage to sustain electrodes  $X_2, X_4, \dots$  on even-numbered rows, respectively. Hereafter, each of the sustain electrodes  $X_1, X_2, X_3, \dots$  or their generic name is a scan electrode  $X_i$ ,  $i$  representing a suffix.

Within a display region 107, the scan electrodes  $Y_i$  and the sustain electrodes  $X_i$  form rows extending in parallel in the horizontal direction, and the address electrodes  $A_j$  form columns extending in the vertical direction. The scan electrodes  $Y_i$  and the sustain electrodes  $X_i$  are alternately and adjacently arranged in the vertical direction. Ribs 106 have a stripe rib structure provided between the address electrodes  $A_j$ .

The scan electrodes  $Y_i$  and the address electrodes  $A_j$  form a two-dimensional matrix with  $i$  rows and  $j$  columns. A display cell  $C_{ij}$  is formed of an intersection of the scan electrode  $Y_i$  and the address electrode  $A_j$  and the sustain electrode  $X_i$  correspondingly adjacent thereto. This display cell  $C_{ij}$  corresponds to a pixel, so that the display region 107 can display a two-dimensional image. The configuration of the display cell  $C_{ij}$  is the same as that in the above-described Figs. 35A to 35C. Further, the frame of an image is the same as that in the description of the above-described Fig. 36.



In this plasma display device, a mode changeover switch 112 is provided which changes between a high image quality mode 114 and a low power mode 115. With the switch 112, a user can make a change between the two modes. The switch 112 may be composed of hardware such as a relay, semiconductor device, remote controller, or the like, or software such as a decision statement of a program or the like. The switch 112 may also be changed by an operation element 113. The result selected by the mode changeover switch 112 is sent to a microcomputer 111. The microcomputer 111 controls the control circuit section 101 based on the selection result.

When the high image quality mode 114 is selected by the mode changeover switch 112, the sustain electrode sustain circuit 103a, the sustain electrode sustain circuit 103b, the scan electrode sustain circuit 104a, and the scan electrode sustain circuit 104b operate in the high image quality mode (second sustain drive mode) by the signal outputted from the control circuit section 101. In the high image quality mode, as shown in Fig. 2, sustain discharge pulses to all adjacent electrodes repeatedly rise or fall at different timings. The use of the high image quality mode can prevent charges on the sustain electrodes and scan electrodes that perform sustain discharges from diffusing to adjacent electrodes, so that high definition video can be displayed with high

image quality with less noise and so on. The detailed description thereof will be made later with reference to Fig. 12. The details of the sustain discharge pulses in Fig. 2 will also be described later.

On the other hand, when the low power mode 115 is selected by the mode changeover switch 112, the sustain electrode sustain circuit 103a, the sustain electrode sustain circuit 103b, the scan electrode sustain circuit 104a, and the scan electrode sustain circuit 104b operate in the low power mode (first sustain drive mode) by the signal outputted from the control circuit section 101. In the low power mode, as shown in Fig. 3, sustain discharge pulses to predetermined adjacent electrodes rise or fall in the same direction at the same time. For example, sustain discharge pulses to a scan electrode  $Y_{n-1}$  and a sustain electrode  $X_n$  rise at the same time and then fall at the same time. When voltages change in the same direction at the same time between the adjacent electrodes as described above, the current flowing through the capacitance between the adjacent electrodes is little. Accordingly, the power loss that is caused by charge to/discharge from the capacitance between the adjacent electrodes is also little. The details of the sustain discharge pulses in Fig. 3 will also be described later.

In the high image quality mode, as shown in Fig. 2, the rising or falling timings of sustain discharge pulses are different between adjacent electrodes, thus increasing the amount of charges for charging/discharging the capacitance between the adjacent electrodes. This results in increases in power of the sustain electrode sustain circuits 103a and 103b and the scan electrode sustain circuits 104a and 104b, leading to high power consumption as compared to that in the low power mode. In contrast to this, in the low power mode, as shown in Fig. 3, sustain discharge pulses to, for example, the scan electrode  $Y_{n-1}$  and the sustain electrode  $X_n$  rise at the same time and then fall at the same time. In this case, since there is no potential difference between the adjacent electrodes, no current flows via the capacitance between the adjacent electrodes, so that the power consumption can be reduced.

The use of this embodiment allows a change to be made between the low power mode with low power consumption (first sustain drive mode) and the high image quality mode capable of high image quality display (second sustain drive mode) for use in accordance with the selection on the user side of the plasma display device.

It should be noted that in this embodiment, the numbers of sustain discharge pulses at the time of maximum load (white screen display) in both the first

sustain drive mode (low power mode) and the second sustain drive mode (high image quality mode) are set to be equal.

Fig. 2 shows sustain discharge pulses during the sustain period  $T_s$  (Fig. 36) in the high image quality mode 114 in Fig. 1. One cycle of the sustain discharge pulse is composed of a period  $T_A$  and a period  $T_B$ , and this cycle is repeated.

The period  $T_A$  will be described. First, at time  $t_1$ , a cathode potential  $V_{s2}$  is applied to the sustain electrodes  $X_{n-1}$  and  $X_{n+1}$  on odd-numbered rows, and the cathode potential  $V_{s2}$  of the scan electrodes  $Y_{n-1}$  and  $Y_{n+1}$  on odd-numbered rows is sustained. Further, an anode potential  $V_{s1}$  of the sustain electrode  $X_n$  on an even-numbered row is sustained, and the cathode potential  $V_{s2}$  of the scan electrode  $Y_n$  on an even-numbered row is sustained.

Subsequently, at time  $t_2$ , the anode potential  $V_{s1}$  is applied to the scan electrodes  $Y_{n-1}$  and  $Y_{n+1}$  on the odd-numbered rows. This applies a high voltage respectively between the sustain electrode  $X_{n-1}$  and the scan electrode  $Y_{n-1}$  and between the sustain electrode  $X_{n+1}$  and the scan electrode  $Y_{n+1}$  to perform sustain discharges  $DE_1$ .

Subsequently, at time  $t_3$ , the cathode potential  $V_{s2}$  is applied to the sustain electrode  $X_n$  on an even-numbered row. Subsequently, at time  $t_4$ , the anode potential  $V_{s1}$  is applied to the scan electrode

$Y_n$  on an even-numbered row. This applies a high voltage between the sustain electrode  $X_n$  and the scan electrode  $Y_n$  to perform a sustain discharge DE2. A period  $T_E$  here is a time period during which both the scan electrode  $Y_{n-1}$  on the odd-numbered row and the sustain electrode  $X_n$  on the even-numbered row are at the anode potential  $V_{s1}$ , and needs to be 500 ns or less.

Subsequently, at time  $t_5$ , the cathode potential  $V_{s2}$  is applied to the scan electrode  $Y_n$  on the even-numbered row. Subsequently, at time  $t_6$ , the anode potential  $V_{s1}$  is applied to the sustain electrode  $X_n$  on the even-numbered row. This applies a high voltage between the sustain electrode  $X_n$  and the scan electrode  $Y_n$  to perform a sustain discharge DE3.

Subsequently, at time  $t_7$ , the cathode potential  $V_{s2}$  is applied to the scan electrodes  $Y_{n-1}$  and  $Y_{n+1}$  on the odd-numbered rows. Subsequently, at time  $t_8$ , the anode potential  $V_{s1}$  is applied to the sustain electrodes  $X_{n-1}$  and  $X_{n+1}$  on the odd-numbered rows. This applies a high voltage respectively between the sustain electrode  $X_{n-1}$  and the scan electrode  $Y_{n-1}$  and between the sustain electrode  $X_{n+1}$  and the scan electrode  $Y_{n+1}$  to perform sustain discharges DE4.

During the period  $T_B$ , the voltage waveforms at the sustain electrodes  $X_{n-1}$  and  $X_{n+1}$  on the odd-numbered rows and the voltage waveform at the sustain electrode  $X_n$  on the even-numbered row are exchanged,

and the voltage waveforms at the scan electrodes  $Y_{n-1}$  and  $Y_{n+1}$  on the odd-numbered rows and the voltage waveform at the scan electrode  $Y_n$  on the even-numbered row are exchanged, with respect to the period  $T_A$ .

Fig. 3 shows sustain discharge pulses during the sustain period  $T_s$  (Fig. 36) in the low power mode 115 in Fig. 1. The sustain discharge pulses are the same as those in the above-described Fig. 38. First, at time  $t_1$ , the cathode potential  $V_{s2}$  is applied to the sustain electrodes  $X_{n-1}$  and  $X_{n+1}$  on the odd-numbered rows, and the anode potential  $V_{s1}$  is applied to the scan electrodes  $Y_{n-1}$  and  $Y_{n+1}$  on the odd-numbered rows. Further, the anode potential  $V_{s1}$  is applied to the sustain electrode  $X_n$  on the even-numbered row, and the cathode potential  $V_{s2}$  is applied to the scan electrode  $Y_n$  on the even-numbered row. This applies a high voltage respectively between the sustain electrode  $X_{n-1}$  and the scan electrode  $Y_{n-1}$ , between the sustain electrode  $X_n$  and the scan electrode  $Y_n$ , and between the sustain electrode  $X_{n+1}$  and the scan electrode  $Y_{n+1}$  to perform sustain discharges DE.

Subsequently, at time  $t_2$ , the anode potential  $V_{s1}$  is applied to the sustain electrodes  $X_{n-1}$  and  $X_{n+1}$  on the odd-numbered rows, and the cathode potential  $V_{s2}$  is applied to the scan electrodes  $Y_{n-1}$  and  $Y_{n+1}$  on the odd-numbered rows. Further, the cathode potential  $V_{s2}$  is applied to the sustain electrode  $X_n$

on the even-numbered row, and the anode potential  $V_{s1}$  is applied to the scan electrode  $Y_n$  on the even-numbered row. This applies a high voltage respectively between the sustain electrode  $X_{n-1}$  and the scan electrode  $Y_{n-1}$ , between the sustain electrode  $X_n$  and the scan electrode  $Y_n$ , and between the sustain electrode  $X_{n+1}$  and the scan electrode  $Y_{n+1}$  to perform sustain discharges DE. The above operation, as one cycle TT, is repeated thereafter.

-Second Embodiment-

Fig. 4 is a diagram showing the configuration of a plasma display device according to a second embodiment of the present invention. This embodiment has basically the same configuration as that of the first embodiment (Fig. 1), and the description will be made on different points.

In this embodiment, a mode changeover switch 112 is provided which changes between a high image quality mode 114 and a high luminance mode 116. Further, a power supply circuit 117 supplies a sustain discharge voltage  $V_s$  via a power supply current detection circuit 118 to sustain electrode sustain circuits 103a and 103b and scan electrode sustain circuits 104a and 104b. The power supply current detection circuit 118 detects a power supply current  $I_s$  to be supplied to the sustain electrode sustain circuits 103a and 103b and the scan electrode sustain circuits 104a and 104b and supplies the

detection result to a microcomputer 111. The microcomputer 111 controls the number of sustain discharge pulses that is set by a control circuit section 101, based on the above power supply current  $I_s$  so that the above power supply current  $I_s$  becomes a predetermined value or less.

The mode changeover switch 112 allows a change to be made between the high image quality mode 114 and the high luminance mode 116 on a user side. For example, when the high image quality mode 114 is selected, the selection result is transmitted to the microcomputer 111, which controls the control circuit section 101 to make setting to generate the sustain discharge pulses in Fig. 2.

On the other hand, when the high luminance mode 116 is selected, the selection result is transmitted to the microcomputer 111, which controls the control circuit section 101 to make setting to generate the sustain discharge pulses in Fig. 3. As shown in Fig. 3, the operation waveforms in the high luminance mode 116, which are the same as the operation waveforms in the low power mode 115 shown in Fig. 1, repeat rising and falling at the same time at predetermined adjacent electrodes. In the high luminance mode 116, the operation waveforms repeat rising and falling at the same time at the adjacent scan electrode  $Y_{n-1}$  and sustain electrode  $X_n$ . As a result of this, the charge/discharge current flowing through the



capacitance between the adjacent electrodes can be reduced. Consequently, the power consumption per the number of sustain discharge pulses can be made low as compared to the high image quality mode shown in Fig. 2.

Since the number of sustain discharge pulses is controlled so that the power supply current  $I_s$  becomes a predetermined value or less by the operations of the power supply current detection circuit 118 and the microcomputer 111, the number of sustain discharge pulses at the time of maximum current (at the time of maximum load such as the entire white display) can be made larger in the high luminance mode 116 with a low power consumption per the predetermined number of sustain discharge pulses than in the high image quality mode 114. Consequently, the luminance of an image at the time of maximum load such as the entire white display can be made higher in the high luminance mode 116 than in the high image quality mode 114.

The use of this embodiment allows a change to be made between the high luminance mode capable of high luminance display and the high image quality mode capable of high image quality display for use in accordance with a selection on the user side of the plasma display device. Consequently, a selection can be made between the high luminance mode and the high image quality mode in accordance with the ambient

brightness, definition of an image to be displayed, or the like.

Fig. 5 shows a configuration example of the power supply current detection circuit 118 in Fig. 4. A terminal 119 is connected to the power supply circuit 117 in Fig. 4, and a terminal 120 is connected to the sustain circuits 103a, 103b, 104a, and 104b in Fig. 4. A resistor 122 is connected between the terminal 119 and the terminal 120 so that the power supply current  $I_s$  flows therethrough. A differential circuit 123 has an inverting terminal connected to the terminal 120 and a non-inverting terminal connected to the terminal 119 and outputs a differential signal (a voltage corresponding to the power supply current  $I_s$ ) to the microcomputer 111 in Fig. 4 via a terminal 121. For example, the number of sustain discharge pulses is controlled so that an average power supply current  $I_s$  per unit time becomes a predetermined value or less. Note that it is also adoptable to detect the power in place of the current to control the number of sustain discharge pulses.

Fig. 6 shows voltage waveforms at a sustain electrode X, a scan electrode Y, and an address electrode A in the high image quality mode in Fig. 4. Corresponding to Fig. 36, subframes SF1 and SF2 are shown. Each subframe is composed of a reset period  $T_r$ , an address period  $T_a$ , and a sustain period (sustain discharge period)  $T_s$ . During the sustain

period  $T_s$ , the sustain discharge pulses in the high image quality mode (Fig. 2) are generated in a period  $T_1$ .

Fig. 7 shows voltage waveforms at the sustain electrode X, the scan electrode Y, and the address electrode A in the high luminance mode in Fig. 4. Fig. 7 is basically the same as Fig. 6, but during the sustain period  $T_s$ , the sustain discharge pulses in the high luminance mode (Fig. 3) are generated in a period  $T_2$ . The sustain discharge pulse period  $T_2$  in the high luminance mode is longer than the sustain discharge pulse period  $T_1$  in the high image quality mode in Fig. 6. In other words, the number of sustain discharge pulses in the high luminance mode in Fig. 7 is larger than that in the high image quality mode in Fig. 6. It should be noted that the numbers of sustain discharge pulses are controlled so that the power consumptions in the high luminance mode and the high image quality mode are the same.

#### -Third Embodiment-

Fig. 8 is a diagram showing the configuration of a plasma display device according to a third embodiment of the present invention. This embodiment has basically the same configuration as that of the second embodiment (Fig. 4), and thus the description will be made on different points.

In this embodiment, a mode changeover switch 112 allows a change to be made among three modes, that is,

a high image quality mode 114, a low power mode 115, and a high luminance mode 116 on a user side. The plasma display device is operated by the sustain discharge pulses shown in Fig. 2 in the high image quality mode 114 and operated by the sustain discharge pulses shown in Fig. 3 in the low power mode 115 and high luminance mode 116. In the low power mode 115, as shown in Fig. 6, the number of sustain discharge pulses T1 at the time of maximum load is set to be equal to that in the high image quality mode 114. Besides, in the high luminance mode 116, as shown in Fig. 7, the number of sustain discharge pulses T2 at the time of maximum load is set to be larger than the number of pulses T1 in the high image quality mode 114 under the condition where the power supply current  $I_s$  becomes a predetermined value or less.

The use of this embodiment allows a selection of an appropriate mode in consideration of the ambient brightness, definition of an image to be displayed, or the like on the user side.

#### -Fourth Embodiment-

Fig. 9 is a diagram showing the configuration of a plasma display device according to a fourth embodiment of the present invention. This embodiment has basically the same configuration as that of the third embodiment (Fig. 8), and the description will be made on different points.

In this embodiment, a brightness detection circuit 124 for detecting the ambient brightness is provided to automatically change a mode changeover switch 112 in accordance with the ambient brightness. As a result of this, when the environment of the plasma display device is bright, a high luminance mode (first sustain drive mode) 116 is automatically selected, and when the environment of the plasma display device is dark, a high image quality mode (second sustain drive mode) 114 is automatically selected. Operations in the modes are the same as those in the third embodiment.

It should be noted that the detection result of the brightness detection circuit 124 for detecting the ambient brightness is supplied to the mode changeover switch 112 in this plasma display device, but may be supplied once to the microcomputer 111 for processing so that the microcomputer 111 may change the mode changeover switch 112. The brightness detection circuit 124 can be composed of, for example, a phototransistor.

The use of the plasma display device according to this embodiment allows an appropriate display mode (sustain drive mode) to be automatically selected in accordance with the ambient brightness.

#### -Fifth Embodiment-

Fig. 10 is a diagram showing the configuration of a plasma display device according to a fifth

embodiment of the present invention. This embodiment has basically the same configuration as that of the fourth embodiment (Fig. 9), and the description will be made on different points.

In the plasma display device of this embodiment, the detection result of a brightness detection circuit 124 for detecting the ambient brightness and the detection result of an image detection circuit 125 for detecting the frequency component, resolution, luminance level, and so on of a video based on an input video signal IMG are inputted into a microcomputer 111. The microcomputer 111 processes the above detection results and automatically changes between the high image quality mode (second sustain drive mode) 114 and the high luminance mode (first sustain drive mode) 116 in accordance with the ambient brightness, frequency component of a display image, resolution (definition), and brightness.

For example, the frequency component of a video is detected based on the input video signal IMG, so that when its high frequency component is at a predetermined value or more, the device is operated in the high image quality mode 114 because the video is fine, and when the high frequency component is at a value less than the predetermined value, the device is operated in the high luminance mode 116 because the video is rough.

Further, the resolution of a video is detected based on the input video signal IMG, so that for a low resolution, the device is operated in the high luminance mode 116, and for a high resolution, the device is operated in the high image quality mode 114. The detection of the resolution can be performed by, for example, counting the number of horizontal synchronization signals to detect the number of lines in one screen.

Further, the luminance level of a video is detected based on the input video signal IMG, so that for a high luminance level, the device is operated in the high luminance mode 116, and for a low luminance level, the device is operated in the high image quality mode 114.

As a result of this, the plasma display device of this embodiment can comprehensively judge the ambient brightness, frequency component of a display video, resolution, and luminance level and automatically select the high image quality mode (second sustain drive mode) 114 or the high luminance mode (first sustain drive mode) 116. Besides, the microcomputer 111 may change between the high image quality mode 114 and the high luminance mode 116 giving priority to either the output of the image detection circuit 125 or the output of the brightness detection circuit 124.

It should be noted that an image processing circuit 126 inputs the input video signal IMG thereinto, performs image processing such as color control, contrast control, and so on for the signal, and outputs the resulting signal to the control circuit section 101. The control circuit section 101 performs display processing based on the input video signal.

The control method of the above high image quality mode will be described in detail below.

-Sixth Embodiment-

Fig. 11 is a cross-sectional view of a progressive method plasma display. On a glass substrate 201, a display cell of a sustain electrode  $X_{n-1}$  and a scan electrode  $Y_{n-1}$ , a display cell of a sustain electrode  $X_n$  and a scan electrode  $Y_n$ , a display cell of a sustain electrode  $X_{n+1}$  and a scan electrode  $Y_{n+1}$ , and so on are formed. Between the display cells, light shields 203 are provided. A dielectric layer 202 is provided to cover the light shields 203 and the electrodes  $X_i$  and  $Y_i$ . A protective film 208 is provided on the dielectric layer 202.

Under a glass substrate 207, an address electrode 206 and a dielectric layer 205 are provided. A discharge space 204 is provided between the protective film 208 and the dielectric layer 205 and has a Ne+Xe Penning gas or the like sealed therein.



Discharged light in the display cell is reflected by the phosphor 1218 (Fig. 35C) and passes through the glass substrate 201 for display.

In the progressive method, the interval between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ , the interval between the electrodes  $X_n$  and  $Y_n$ , and the interval between the electrodes  $X_{n+1}$  and  $Y_{n+1}$ , being the respective pairs of electrodes constituting the display cells, are small, so that discharges can be performed. Besides, the interval between the electrodes  $Y_{n-1}$  and  $X_n$  and the interval between the electrodes  $Y_n$  and  $X_{n+1}$ , the intervals existing between different display cells, are large, so that discharge is not performed. In other words, each electrode can perform a sustain discharge only with the adjacent electrode on one side thereof.

The frame of an image displayed by the plasma display is the same as that in the aforementioned Fig. 36. In Fig. 36, first, during the reset period  $T_r$ , a predetermined voltage is applied between the scan electrodes  $Y_i$  and the sustain electrodes  $X_i$  to perform a total write and a total erase of charges, thereby erasing previous display contents and forming predetermined wall charges.

Then, during the address period  $T_a$ , a pulse at a positive potential (lighting selection voltage) is applied to the address electrode  $A_j$  and a pulse at a cathode potential  $V_{s2}$  is applied to a desired scan

electrode  $Y_i$  by a sequential scan. These pulses cause an address discharge between the address electrode  $A_j$  and the scan electrode  $Y_i$  to address a display cell (select for lighting).

Subsequently, during the sustain period (sustain discharge period)  $T_s$ , a predetermined voltage is applied between the sustain electrodes  $X_i$  and the scan electrodes  $Y_i$  to perform a sustain discharge between the sustain electrode  $X_i$  and the scan electrode  $Y_i$  which correspond to the display cell addressed during the address period  $T_a$  for light emission.

Fig. 12 is a timing chart showing a driving method during the sustain period  $T_s$  of the progressive method plasma display. The electrodes  $X_{n-1}$ ,  $Y_{n-1}$ ,  $X_n$ ,  $Y_n$ ,  $X_{n+1}$ ,  $Y_{n+1}$ ,  $X_{n+2}$ ,  $Y_{n+2}$ , and so on are provided in sequence in order.

First, from time  $t_1$  to time  $t_2$ , first discharges  $DE_1$  are performed between the electrodes  $X_n$  and  $Y_n$  and between electrodes  $X_{n+2}$  and  $Y_{n+2}$ . Subsequently, from time  $t_3$  to time  $t_4$ , second discharges  $DE_2$  are performed between the electrodes  $X_{n-1}$  and  $Y_{n-1}$  and between the electrodes  $X_{n+1}$  and  $Y_{n+1}$ . Subsequently, from time  $t_5$  to time  $t_6$ , third discharges  $DE_3$  are performed between the electrodes  $X_{n-1}$  and  $Y_{n-1}$  and between the electrodes  $X_{n+1}$  and  $Y_{n+1}$ . Subsequently, from time  $t_7$  to time  $t_8$ , fourth discharges  $DE_4$  are performed between the electrodes  $X_n$  and  $Y_n$  and

between the electrodes  $X_{n+2}$  and  $Y_{n+2}$ . The sustain discharges are repeated with the first to fourth discharges DE1 to DE4 as one cycle. This can prevent negative charges (electrons) during the discharges from diffusing to adjacent electrodes.

Here, the same voltage is applied to the sustain electrodes  $X_{n-1}$ ,  $X_{n+1}$ , and the like on the odd-numbered rows, the same voltage is applied to the sustain electrodes  $X_n$ ,  $X_{n+2}$ , and the like on the even-numbered rows, the same voltage is applied to the scan electrodes  $Y_{n-1}$ ,  $Y_{n+1}$ , and the like on the odd-numbered rows, and the same voltage is applied to the scan electrodes  $Y_n$ ,  $Y_{n+2}$ , and the like on the even-numbered rows.

During the sustain period  $T_s$ , even-numbered electrode pairs and odd-numbered electrode pairs, out of electrode pairs of a plurality of display cells which perform display during the sustain period  $T_s$ , perform discharges for light emission at different timings. For example, the odd-numbered electrode pairs perform the discharges DE1 and DE4, and, at a timing different therefrom, the even-numbered electrode pairs perform the discharges DE2 and DE3.

Further, the discharge for light emission of one pair of the even-numbered electrode pair and the odd-numbered electrode pair is performed first and then the discharge for light emission of the other pair is performed. In this event, the applied voltages to

the one electrode pair are sustained from the start of the discharge for light emission between the one electrode pair to the end of the discharge for light emission between the other electrode pair.

-First Discharge-

Figs. 13A to 13C are diagrams for explaining conditions of the first discharge DE1 in Fig. 12. The display cell of the electrodes Xn and Yn is addressed (selected to light up) during the address period Ta (Fig. 36), the cathode voltage Vs2 is applied to the electrode Xn, and the anode voltage Vs1 is applied to the electrode Yn during the sustain period Ts (Fig. 36), thereby causing a discharge between the electrodes Xn and Yn. In this event, if the display cell of the electrodes Xn-1 and Yn-1 is addressed, positive wall charges are formed on the adjacent electrode Yn-1, and if the display cell of the electrodes Xn+1 and Yn+1 is addressed, negative wall charges are formed on the adjacent electrode Xn+1. The same voltage is applied to the sustain electrodes Xn-1 and Xn+1 on the odd-numbered rows, and the same voltage is applied to the scan electrodes Yn-1 and Yn+1 on the odd-numbered rows.

Fig. 13A is a diagram showing the voltages to the adjacent electrodes Yn-1 and Xn+1 set to  $(Vs1 + Vs2)/2$  when a discharge is caused between the electrodes Xn and Yn. In this case, the wall charges on the electrodes Xn and Yn never diffuse to the

adjacent electrodes  $Y_{n-1}$  and  $X_{n+1}$ , thereby preventing error display.

Fig. 13B is a diagram showing the voltages to the adjacent electrodes  $Y_{n-1}$  and  $X_{n+1}$  set to the cathode voltage  $V_{s2}$  when a discharge is caused between the electrodes  $X_n$  and  $Y_n$ . In this case, the negative wall charges on the adjacent electrode  $X_{n+1}$  diffuse onto the electrode  $Y_n$ . Therefore, the adjacent electrode  $X_{n+1}$  needs to have a voltage higher than the cathode voltage  $V_{s2}$ . On the other hand, the wall charges on the electrodes  $X_n$  and  $Y_n$  never diffuse onto the electrode  $Y_{n-1}$ . Therefore, the adjacent electrode  $Y_{n-1}$  only needs to have a voltage equal to or higher than the cathode voltage  $V_{s2}$ .

Fig. 13C is a diagram showing the voltages to the adjacent electrodes  $Y_{n-1}$  and  $X_{n+1}$  set to the anode voltage  $V_{s1}$  when a discharge is caused between the electrodes  $X_n$  and  $Y_n$ . In this case, the negative wall charges on the adjacent electrode  $X_n$  diffuse onto the adjacent electrode  $Y_{n-1}$ . Therefore, the adjacent electrode  $Y_{n-1}$  needs to have a voltage lower than the anode voltage  $V_{s1}$ . On the other hand, when the negative charges exist on the electrode  $X_{n+1}$ , the negative wall charges on the electrode  $X_n$  never diffuse over the electrode  $Y_n$  onto the electrode  $X_{n+1}$ . However, if the display cell of the electrodes  $X_{n+1}$  and  $Y_{n+1}$  is not addressed, no wall charge exists on the electrodes  $X_{n+1}$  and  $Y_{n+1}$ . In this case, the

negative wall charges on the electrode  $X_n$  diffuse over the electrode  $Y_n$  onto the electrode  $X_{n+1}$ . This may cause the display cell of the electrodes  $X_{n+1}$  and  $Y_{n+1}$  to light up in error later. Therefore, the adjacent electrode  $X_{n+1}$  needs to have a voltage lower than the anode voltage  $V_{s1}$ .

Similarly, in Fig. 13B, if the display cell of the electrodes  $X_{n-1}$  and  $Y_{n-1}$  is not addressed, no wall charge exists on the electrodes  $X_{n-1}$  and  $Y_{n-1}$ . Also in this case, it can be reasoned that the positive wall charges on the electrode  $Y_n$  diffuse over the electrode  $X_n$  onto the electrode  $Y_{n-1}$ . Actually, however, the positive wall charges are larger in mass than the negative wall charges, and thus are hard to diffuse as compared to the negative wall charges. Therefore, in Fig. 13B, the positive wall charges on the electrode  $Y_n$  never diffuse over the electrode  $X_n$  onto the electrode  $Y_{n-1}$ .

The foregoing conditions will be explained together. When the cathode voltage  $V_{s2}$  is applied to the electrode  $X_n$ , and the anode voltage  $V_{s1}$  is applied to the electrode  $Y_n$  to cause a discharge between the electrodes  $X_n$  and  $Y_n$ , an applied voltage  $V_{yn-1}$  to the adjacent electrode  $Y_{n-1}$  only needs to be set within the following range. For example, in Fig. 12, the voltage  $V_{yn-1} = (V_{s1} + V_{s2})/2$ .

$$V_{s2} \leq V_{yn-1} < V_{s1}$$

Further, an applied voltage  $V_{xn+1}$  to the adjacent electrode  $X_{n+1}$  only needs to be set within the following range. For example, in Fig. 12, the voltage  $V_{xn+1} = (V_{s1} + V_{s2})/2$ .

$$V_{s2} < V_{xn+1} < V_{s1}$$

As described above, in this event, when lighting is caused by sustain (sustain discharge) between the adjacent electrodes  $X_{n-1}$  and  $Y_{n-1}$ , the polarity of the wall charges on the electrode  $Y_{n-1}$ , generated by the previous sustain between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ , becomes positive. Similarly, when lighting is caused by sustain between the adjacent electrodes  $X_{n+1}$  and  $Y_{n+1}$ , the polarity of the wall charges on the electrode  $X_{n+1}$ , generated by the previous sustain between the electrodes  $X_{n+1}$  and  $Y_{n+1}$ , becomes negative. Such sustain discharge voltage prevents the negative wall charges on the electrode  $X_n$  from diffusing to the electrode  $Y_{n-1}$  or the electrode  $X_{n+1}$ .

#### -Second Discharge-

Figs. 14A to 14C are diagrams for explaining conditions of the second discharge DE2 in Fig. 12. The display cell of the electrodes  $X_{n-1}$  and  $Y_{n-1}$  is addressed (selected to light up) during the address period  $T_a$  (Fig. 36), the cathode voltage  $V_{s2}$  is applied to the electrode  $X_{n-1}$ , and the anode voltage  $V_{s1}$  is applied to the electrode  $Y_{n-1}$  during the sustain period  $T_s$  (Fig. 36), thereby causing a discharge between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ . In

this event, if the display cell of the electrodes  $X_{n-2}$  and  $Y_{n-2}$  is addressed, negative wall charges are formed on the electrode  $Y_{n-2}$ , and if the display cell of the electrodes  $X_n$  and  $Y_n$  is addressed, positive wall charges are formed on the electrode  $X_n$ . The same voltage is applied to the sustain electrodes  $X_{n-2}$  and  $X_n$  on the even-numbered rows, and the same voltage is applied to the scan electrodes  $Y_{n-2}$  and  $Y_n$  on the even-numbered rows.

Fig. 14A is a diagram showing the voltages to the adjacent electrodes  $Y_{n-2}$  and  $X_n$  set to  $(V_{s1} + V_{s2})/2$  when a discharge is caused between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ . In this case, the wall charges on the electrodes  $X_{n-1}$  and  $Y_{n-1}$  never diffuse to the adjacent electrodes  $Y_{n-2}$  and  $X_n$ , thereby preventing error display.

Fig. 14B is a diagram showing the voltages to the adjacent electrodes  $Y_{n-2}$  and  $X_n$  set to the cathode voltage  $V_{s2}$  when a discharge is caused between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ . In this case, the charges on the electrodes  $X_{n-1}$  and  $Y_{n-1}$  never diffuse onto the electrode  $X_n$ . Note that since positive wall charges are formed both on the electrodes  $Y_{n-1}$  and  $X_n$ , no charge transfers between the electrodes  $Y_{n-1}$  and  $X_n$ . Besides, even when the display cell of the electrodes  $X_n$  and  $Y_n$  is not addressed and thus no wall charge exists on the electrodes  $X_n$  and  $Y_n$ , the positive wall charges on the electrode  $Y_{n-1}$  never



diffuse onto the electrode  $X_n$ . In this event, no negative charge exists on the electrode  $X_n$ . Therefore, the adjacent electrode  $X_n$  only needs to have a voltage equal to or higher than the cathode voltage  $V_{s2}$ . On the other hand, the charges on the electrodes  $X_{n-1}$  and  $Y_{n-1}$  never diffuse to the adjacent electrode  $Y_{n-2}$ . Note that the positive wall charges on the electrode  $Y_{n-1}$  are larger in mass than the negative wall charges, and thus never diffuse over the electrode  $X_{n-1}$  onto the electrode  $Y_{n-2}$ . Therefore, the adjacent electrode  $Y_{n-2}$  only needs to have a voltage equal to or higher than the cathode voltage  $V_{s2}$ .

Fig. 14C is a diagram showing the voltages to the adjacent electrodes  $Y_{n-2}$  and  $X_n$  set to the anode voltage  $V_{s1}$  when a discharge is caused between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ . In this case, the charges on the electrodes  $X_{n-1}$  and  $Y_{n-1}$  never diffuse onto the adjacent electrode  $Y_{n-2}$ . Note that since negative wall charges are formed both on the electrodes  $X_{n-1}$  and  $Y_{n-2}$ , no charge transfers between the electrodes  $X_{n-1}$  and  $Y_{n-2}$ . Besides, even when the display cell of the electrodes  $X_{n-2}$  and  $Y_{n-2}$  is not addressed and thus no wall charge exists on the electrodes  $X_{n-2}$  and  $Y_{n-2}$ , the negative wall charges on the electrode  $X_{n-1}$  never diffuse onto the electrodes  $Y_{n-2}$ . Therefore, the adjacent electrode  $Y_{n-2}$  needs to have a voltage equal to or lower than

the anode voltage  $V_{s1}$ . On the other hand, since the electrodes  $Y_{n-1}$  and  $X_n$  are at the same potential, the negative wall charges on the electrode  $X_{n-1}$  diffuse to the electrodes  $Y_{n-1}$  and the electrode  $X_n$  adjacent thereto. In this event, if the positive wall charges exist or do not exist on the electrode  $X_n$  in response to the addressing of the display cell of the electrodes  $X_n$  and  $Y_n$ , the negative wall charges on the electrode  $X_{n-1}$  diffuse onto the electrode  $X_n$ . Therefore, the adjacent electrode  $X_n$  needs to have a voltage lower than the anode voltage  $V_{s1}$ .

The foregoing conditions will be explained together. When the cathode voltage  $V_{s2}$  is applied to the electrode  $X_{n-1}$ , and the anode voltage  $V_{s1}$  is applied to the electrode  $Y_{n-1}$  to cause a discharge between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ , an applied voltage  $V_{xn}$  to the electrode  $X_n$  only needs to be set within the following range. For example, in Fig. 12, the voltage  $V_{xn} = V_{s2}$ .

$$V_{s2} \leq V_{xn} < V_{s1}$$

Similarly, when the cathode voltage  $V_{s2}$  is applied to the electrode  $X_{n-1}$ , and the anode voltage  $V_{s1}$  is applied to the electrode  $Y_{n-1}$  to cause a discharge between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ , an applied voltage  $V_{yn}$  to the electrode  $Y_{n-2}$  ( $Y_n$ ) only needs to be set within the following range. For example, in Fig. 12, the voltage  $V_{yn} = V_{s1}$ .

$$V_{s2} \leq V_{yn} \leq V_{s1}$$

In this event, when lighting is caused by sustain (sustain discharge) between the electrodes  $X_n$  and  $Y_n$ , the polarity of the wall charges on the electrode  $X_n$ , generated by the previous sustain between the electrodes  $X_n$  and  $Y_n$ , becomes positive, and the polarity of the wall charges on the electrode  $Y_n$  becomes negative. This prevents the negative wall charges on the electrode  $X_{n-1}$  from diffusing to the electrode  $X_n$  or  $Y_{n-2}$ .

-Third Discharge-

Figs. 15A to 15C are diagrams for explaining conditions of the third discharge DE3 in Fig. 12. The display cell of the electrode  $X_{n-1}$  and the electrode  $Y_{n-1}$  is addressed (selected to light up) during the address period  $T_a$  (Fig. 36), the anode voltage  $V_{s1}$  is applied to the electrode  $X_{n-1}$ , and the cathode voltage  $V_{s2}$  is applied to the electrode  $Y_{n-1}$  during the sustain period  $T_s$  (Fig. 36), thereby causing a discharge between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ . In this event, if the display cell of the electrodes  $X_{n-2}$  and  $Y_{n-2}$  is addressed, negative wall charges are formed on the electrode  $Y_{n-2}$ , and if the display cell of the electrodes  $X_n$  and  $Y_n$  is addressed, positive wall charges are formed on the electrode  $X_n$ . The same voltage is applied to the sustain electrodes  $X_{n-2}$  and  $X_n$  on the even-numbered rows, and the same voltage is applied to the scan electrodes  $Y_{n-2}$  and  $Y_n$  on the even-numbered rows.

Fig. 15A is a diagram showing the voltages to the adjacent electrodes  $Y_{n-2}$  and  $X_n$  set to  $(V_{s1} + V_{s2})/2$  when a discharge is caused between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ . In this case, the wall charges on the electrodes  $X_{n-1}$  and  $Y_{n-1}$  never diffuse to the adjacent electrodes  $Y_{n-2}$  or  $X_n$ , thereby preventing error display.

Fig. 15B is a diagram showing the voltages to the adjacent electrodes  $Y_{n-2}$  and  $X_n$  set to the cathode voltage  $V_{s2}$  when a discharge is caused between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ . In this case, the charges on the electrodes  $X_{n-1}$  and  $Y_{n-1}$  never diffuse onto the electrode  $X_n$ . Note that the positive wall charges on the electrode  $X_{n-1}$  are larger in mass than the negative wall charges, and thus never diffuse over the electrode  $Y_{n-1}$  onto the electrode  $X_n$ . Therefore, the adjacent electrode  $X_n$  only needs to have a voltage equal to or higher than the cathode voltage  $V_{s2}$ . On the other hand, the negative wall charges on the electrode  $Y_{n-2}$  diffuse onto the electrodes  $X_{n-1}$ . Therefore, the adjacent electrode  $Y_{n-2}$  needs to have a voltage higher than the cathode voltage  $V_{s2}$ .

Fig. 15C is a diagram showing the voltages to the adjacent electrodes  $Y_{n-2}$  and  $X_n$  set to the anode voltage  $V_{s1}$  when a discharge is caused between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ . In this case, the negative wall charges on the electrodes  $Y_{n-1}$  diffuse onto the

adjacent electrode  $X_n$ . Therefore, the adjacent electrode  $X_n$  needs to have a voltage lower than the anode voltage  $V_{s1}$ . On the other hand, if negative charges exist on the electrode  $Y_{n-2}$ , the negative wall charges on the electrode  $Y_{n-1}$  never diffuse over the electrode  $X_{n-1}$  onto the electrode  $Y_{n-2}$ . However, if the display cell of the electrodes  $X_{n-2}$  and  $Y_{n-2}$  is not addressed, and thus no wall charge exists on the electrodes  $X_{n-2}$  and  $Y_{n-2}$ , the negative wall charges on the electrode  $Y_{n-1}$  diffuse over the electrode  $X_{n-1}$  onto the electrode  $Y_{n-2}$ . This may cause the display cell of the electrodes  $X_{n-2}$  and  $Y_{n-2}$  to light up in error later. Therefore, the adjacent electrode  $Y_{n-2}$  needs to have a voltage lower than the anode voltage  $V_{s1}$ .

The foregoing conditions will be explained together. When the anode voltage  $V_{s1}$  is applied to the electrode  $X_{n-1}$  and the cathode voltage  $V_{s2}$  is applied to the electrode  $Y_{n-1}$  to cause a discharge between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ , an applied voltage  $V_{xn}$  to the electrode  $X_n$  only needs to be set within the following range. For example, in Fig. 12, the voltage  $V_{xn} = (V_{s1} + V_{s2})/2$ .

$$V_{s2} \leq V_{xn} < V_{s1}$$

Similarly, when the anode voltage  $V_{s1}$  is applied to the electrode  $X_{n-1}$ , and the cathode voltage  $V_{s2}$  is applied to the electrode  $Y_{n-1}$  to cause a discharge between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ , an applied

voltage  $V_{yn}$  to the electrode  $Y_{n-2}$  ( $Y_n$ ) only needs to be set within the following range. For example, in Fig. 12, the voltage  $V_{yn} = (V_{s1} + V_{s2})/2$ .

$$V_{s2} < V_{yn} < V_{s1}$$

In this event, when lighting is caused by sustain (sustain discharge) between the electrodes  $X_n$  and  $Y_n$ , the polarity of the wall charges on the electrode  $X_n$ , generated by the previous sustain between the electrodes  $X_n$  and  $Y_n$ , becomes positive, and the polarity of the wall charges on the electrode  $Y_n$  becomes negative. This prevents the negative wall charges on the electrode  $Y_{n-1}$  from diffusing to the electrode  $X_n$  or  $Y_{n-2}$ .

#### -Fourth Discharge-

Figs. 16A to 16C are diagrams for explaining conditions of the fourth discharge DE4 in Fig. 12. The display cell of the electrodes  $X_n$  and  $Y_n$  is addressed (selected to light up) during the address period  $T_a$  (Fig. 36), the anode voltage  $V_{s1}$  is applied to the electrode  $X_n$ , and the cathode voltage  $V_{s2}$  is applied to the electrode  $Y_n$  during the sustain period  $T_s$  (Fig. 36), thereby causing a discharge between the electrodes  $X_n$  and  $Y_n$ . In this event, if the display cell of the electrodes  $X_{n-1}$  and  $Y_{n-1}$  is addressed, positive wall charges are formed on the adjacent electrode  $Y_{n-1}$ , and if the display cell of the electrodes  $X_{n+1}$  and  $Y_{n+1}$  is addressed, negative wall charges are formed on the adjacent electrode  $X_{n+1}$ .

Fig. 16A is a diagram showing the voltages to the adjacent electrodes  $Y_{n-1}$  and  $X_{n+1}$  set to  $(V_{s1} + V_{s2})/2$  when a discharge is caused between the electrodes  $X_n$  and  $Y_n$ . In this case, the wall charges on the electrodes  $X_n$  and  $Y_n$  never diffuse to the adjacent electrode  $Y_{n-1}$  or  $X_{n+1}$ , thereby preventing error display.

Fig. 16B is a diagram showing the voltages to the adjacent electrodes  $Y_{n-1}$  and  $X_{n+1}$  set to the cathode voltage  $V_{s2}$  when a discharge is caused between the electrodes  $X_n$  and  $Y_n$ . In this case, the charges on the electrodes  $X_n$  and  $Y_n$  never diffuse onto the electrode  $X_{n+1}$ . Note that the positive wall charges on the electrode  $X_n$  are larger in mass than the negative wall charges, and thus never diffuse over the electrode  $Y_n$  onto the electrode  $X_{n+1}$ . Therefore, the adjacent electrode  $X_{n+1}$  only needs to have a voltage equal to or higher than the cathode voltage  $V_{s2}$ . On the other hand, the charges on the electrodes  $X_n$  and  $Y_n$  never diffuse onto the electrode  $Y_{n-1}$ . Note that since the polarity of the wall charges on the electrode  $Y_{n-1}$  is positive, no charge transfers between the electrodes  $X_n$  and  $Y_{n-1}$ . Besides, even when the display cell of the electrodes  $X_{n-1}$  and  $Y_{n-1}$  is not addressed, and thus no wall charge exists on the electrodes  $X_{n-1}$  and  $Y_{n-1}$ , the positive wall charges on the electrode  $X_n$  never diffuse onto the electrode  $Y_{n-1}$ . In this event, no

negative wall charge exists on the electrode  $Y_{n-1}$ . Therefore, the adjacent electrode  $Y_{n-1}$  only needs to have a voltage equal to or higher than the cathode voltage  $V_{s2}$ .

Fig. 16C is a diagram showing the voltages to the adjacent electrodes  $Y_{n-1}$  and  $X_{n+1}$  set to the anode voltage  $V_{s1}$  when a discharge is caused between the electrodes  $X_n$  and  $Y_n$ . In this case, the charges on the electrodes  $X_n$  and  $Y_n$  never diffuse onto the adjacent electrode  $X_{n+1}$ . Note that since the polarity of the wall charges on the electrode  $X_{n+1}$  is negative, no charge transfers between the electrodes  $Y_n$  and  $X_{n+1}$ . Besides, even when the display cell of the electrodes  $X_{n+1}$  and  $Y_{n+1}$  is not addressed, and thus no wall charge exists on the electrodes  $X_{n+1}$  and  $Y_{n+1}$ , the negative wall charges on the electrode  $Y_n$  never diffuse onto the electrode  $X_{n+1}$ . In this event, no positive wall charge exists on the electrode  $X_{n+1}$ . Therefore, the adjacent electrode  $X_{n+1}$  only needs to have a voltage equal to or lower than the anode voltage  $V_{s1}$ . On the other hand, the negative charges on the electrode  $Y_n$  diffuse over the electrode  $X_n$  to the electrode  $Y_{n-1}$ . In this event, if the positive wall charges exist or do not exist on the electrode  $Y_{n-1}$  in response to the addressing of the display cell of the electrodes  $X_{n-1}$  and  $Y_{n-1}$ , the negative wall charges on the electrode  $Y_n$  diffuse over the electrode  $X_n$  onto the electrode  $Y_{n-1}$ . Therefore, the



adjacent electrode  $Y_{n-1}$  needs to have a voltage lower than the anode voltage  $V_{s1}$ .

The foregoing conditions will be explained together. When the anode voltage  $V_{s1}$  is applied to the electrode  $X_n$ , and the cathode voltage  $V_{s2}$  is applied to the electrode  $Y_n$  to cause a discharge between the electrodes  $X_n$  and  $Y_n$ , an applied voltage  $V_{yn-1}$  to the electrode  $Y_{n-1}$  only needs to be set within the following range. For example, in Fig. 12, the voltage  $V_{yn-1} = V_{s2}$ .

$$V_{s2} \leq V_{yn-1} < V_{s1}$$

Besides, an applied voltage  $V_{xn+1}$  to the electrode  $X_{n+1}$  only needs to be set within the following range. For example, in Fig. 12, the voltage  $V_{xn+1} = V_{s1}$ .

$$V_{s2} \leq V_{xn+1} \leq V_{s1}$$

In this event, when lighting is caused by sustain (sustain discharge) between the electrodes  $X_{n-1}$  and  $Y_{n-1}$  adjacent to the electrodes  $X_n$  and  $Y_n$ , the polarity of the wall charges on the electrode  $Y_{n-1}$ , generated by the previous sustain between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ , becomes positive. Similarly, when lighting is caused by sustain between the electrodes  $X_{n+1}$  and  $Y_{n+1}$  adjacent to the electrodes  $X_n$  and  $Y_n$ , the polarity of the wall charges on the electrode  $X_{n+1}$ , generated by the previous sustain between the electrodes  $X_{n+1}$  and  $Y_{n+1}$ , becomes negative. Such voltage waveforms of sustain

discharges prevent the negative wall charges on the electrode  $Y_n$  from diffusing to the electrode  $Y_{n-1}$  or  $X_{n+1}$ .

-Seventh Embodiment-

Fig. 17 is a timing chart showing a driving method during the sustain period  $T_s$  of a progressive method plasma display according to a seventh embodiment of the present invention. The voltage waveforms of sustain discharges in Fig. 17 are basically the same as those in Fig. 12, and thus the following description will be made on different points.

As for the first discharge  $DE_1$ , the cathode voltage  $V_{s2}$  is applied to the electrode  $X_n$ , and the anode voltage  $V_{s1}$  is applied to the electrode  $Y_n$ , thereby causing a discharge between the electrodes  $X_n$  and  $Y_n$ . In this event, the applied voltage  $V_{xn+1}$  to the adjacent electrode  $X_{n+1}$  is changed within the following range.

$$V_{s2} < V_{xn+1} < V_{s1}$$

For example, the voltage  $V_{xn+1}$  is gradually changed from the anode voltage  $V_{s1}$  to the cathode voltage  $V_{s2}$ . This means that the applied voltage to the adjacent electrode may be changed during the discharge within the range of the conditions shown in the sixth embodiment. Note that, during the first discharge  $DE_1$ , the adjacent electrode  $Y_{n-1}$  sustains

the cathode voltage  $V_{s2}$  as from before the first discharge DE1 in this embodiment.

As for the third discharge DE3, the anode voltage  $V_{s1}$  is applied to the electrode  $X_{n+1}$  and the cathode voltage  $V_{s2}$  is applied to the electrode  $Y_{n+1}$ , thereby causing a discharge between the electrodes  $X_{n+1}$  and  $Y_{n+1}$ . In this event, the applied voltage  $V_{yn}$  to the adjacent electrode  $Y_n$  is changed within the following range.

$$V_{s2} < V_{yn} < V_{s1}$$

Note that, during the third discharge DE3, the adjacent electrode  $X_n$  sustains the cathode voltage  $V_{s2}$  as from before the third discharge DE3 in this embodiment.

According to this embodiment, even if the applied voltage to the adjacent electrode is changed during the discharge within the range of the conditions shown in the sixth embodiment, the same effects as those in the first embodiment can be attained. In other words, it is possible to prevent diffusion of charges so as to eliminate error display.

-Eighth Embodiment-

Fig. 18 is a timing chart showing a driving method during the sustain period  $T_s$  of a progressive method plasma display according to an eighth embodiment of the present invention. The voltage waveforms of sustain discharges in Fig. 18 are basically the same as those in Fig. 17 and thus the

following description will be made on different points.

As for the first discharge DE1, the cathode voltage  $V_{s2}$  is applied to the electrode  $X_n$ , and the anode voltage  $V_{s1}$  is applied to the electrode  $Y_n$ , thereby causing a discharge between the electrodes  $X_n$  and  $Y_n$ . In this event, the applied voltage  $V_{xn+1}$  to the adjacent electrode  $X_{n+1}$  is set to  $V_{xn+1} = V_{s1}$ , exceeding the set range  $V_{s2} < V_{xn+1} < V_{s1}$ . In this event, however, a time  $T_E$  during which  $V_{xn+1} = V_{s1}$  is within 500 ns. For example, the time  $T_E$  is 100 ns. After a lapse of the time  $T_E$ , the voltage  $V_{xn+1}$  is set within the range  $V_{s2} < V_{xn+1} < V_{s1}$ .

This applies to the third discharge DE3. During the third discharge DE3, the applied voltage  $V_{yn}$  to the adjacent electrode  $Y_n$  is first set to  $V_{yn} = V_{s1}$  during the time  $T_E$  and then to the range  $V_{s2} < V_{yn} < V_{s1}$ .

According to this embodiment, within 500 ns, even if the voltage to the aforementioned adjacent electrode is  $V_{s1}$ , the negative charges on the electrode  $X_n$  during the period of the first discharge DE1 and the negative charges on the electrode  $Y_{n+1}$  during the period of the third discharge DE3 never diffuse to the electrodes  $X_{n+1}$  and  $Y_n$ , respectively. The reason will be described hereafter with reference to Figs. 19A to 19C and Figs. 20A to 20C.

Figs. 19A to 19C show a problem when the anode voltage  $V_{s1}$  is kept applied to the adjacent electrode  $X_{n+1}$  during the first discharge  $DE1$  in Fig. 18. Figs. 19A to 19C show the state in Fig. 13C with time transition. More specifically, the cathode voltage  $V_{s2}$  is applied to the electrode  $X_n$ , the anode voltage  $V_{s1}$  to the electrode  $Y_n$ , and the anode voltage  $V_{s1}$  to the adjacent electrode  $X_{n+1}$ .

In Fig. 19A, the negative charges on the electrode  $X_n$  start to transfer onto the electrode  $Y_n$  due to the potential difference between the electrodes  $X_n$  and  $Y_n$ . In Fig. 19B, the negative charges on the electrode  $X_n$  further transfer onto the electrode  $Y_n$ . In Fig. 19C, the negative charges on the electrode  $X_n$  further transfer onto the electrode  $Y_n$  to form negative charges on the electrode  $Y_n$ . When a predetermined amount of negative charges are formed on the electrode  $Y_n$ , the negative charges on the electrode  $Y_n$  diffuse to the adjacent electrode  $X_{n+1}$ .

Figs. 20A to 20C show transition of voltage to the adjacent electrode  $X_{n+1}$  during the first discharge  $DE1$  shown in Fig. 18. In Fig. 20A, the cathode voltage  $V_{s2}$  is applied to the electrode  $X_n$ , the anode voltage  $V_{s1}$  is applied to the electrode  $Y_n$ , and the anode voltage  $V_{s1}$  is applied to the adjacent electrode  $X_{n+1}$ . This state is sustained for the time  $T_E$  (within 500 ns). Then, the negative charges on

the electrode  $X_n$  transfer onto the electrode  $Y_n$  as in Fig. 20B. Then, after the time  $T_E$  and before a predetermined amount of negative charges are formed on the electrode  $Y_n$ , as shown in Fig. 20C, the voltage  $V_{Xn+1}$  to the adjacent electrode  $X_{n+1}$  is set within the range  $V_{s2} < V_{Xn+1} < V_{s1}$ . For example, the voltage  $V_{Xn+1} = (V_{s1} + V_{s2})/2$ . This can prevent the negative charges from diffusing onto the electrode  $X_{n+1}$ .

-Ninth Embodiment-

Fig. 21 is a timing chart showing a driving method during the sustain period  $T_s$  of a progressive method plasma display according to a ninth embodiment of the present invention. This embodiment shows the sustain discharge voltage waveforms of repeating the voltage waveforms during the period  $T_T$  shown in the seventh embodiment (Fig. 17) as one cycle. The one cycle  $T_T$  includes the first to fourth discharges  $DE1$  to  $DE4$ .

-Tenth Embodiment-

Fig. 22 is a timing chart showing a driving method during the sustain period  $T_s$  of a progressive method plasma display according to a tenth embodiment of the present invention. A period  $T_A$  is the same as the period  $T_T$  in Fig. 21. In a period  $T_B$  subsequent thereto, in comparison with the period  $T_A$ , the voltage to the sustain electrodes  $X_n$  and the like on the even-numbered rows is exchanged with the voltage

to the sustain electrodes  $X_{n-1}$  and the like on the odd-numbered rows, and the voltage to the scan electrodes  $Y_n$  and the like on the even-numbered rows is exchanged with the voltage to the scan electrodes  $Y_{n-1}$  and the like on the odd-numbered rows. The waveforms during the period  $TT$  composed of a set of the period  $TA$  and the period  $TB$  are repeated as one cycle to form the voltage waveforms of sustain discharges. This embodiment can also prevent, as in the ninth embodiment, the negative charges from diffusing to eliminate error display.

In the ninth embodiment (Fig. 21), in all the periods  $TT$ , the discharges  $DE2$  and  $DE3$  are performed between the electrodes  $X_{n-1}$  and  $Y_{n-1}$  at short intervals, while the discharges  $DE1$  and  $DE4$  are performed between the electrodes  $X_n$  and  $Y_n$  at long intervals. In other words, there occurs unevenness between the intervals of discharges between the electrodes  $X_{n-1}$  and  $Y_{n-1}$  and the intervals of discharges between the electrodes  $X_n$  and  $Y_n$ . In contrast to this, in the tenth embodiment (Fig. 22), the periods  $TA$  and  $TB$  are alternately performed to eliminate the unevenness between the intervals of discharges between the electrodes  $X_{n-1}$  and  $Y_{n-1}$  and the intervals of discharges between the electrodes  $X_n$  and  $Y_n$ .

-Eleventh Embodiment-

Fig. 23 is a timing chart showing a driving method during the sustain period  $T_s$  of a progressive method plasma display according to an eleventh embodiment of the present invention. In the eleventh embodiment, as in the tenth embodiment (Fig. 22), the period  $T_T$  composed of the periods  $T_A$  and  $T_B$  is one cycle. While the voltage waveforms in the seventh embodiment (Fig. 17) are applied to the tenth embodiment, the voltage waveforms in the eighth embodiment (Fig. 18) are applied to the eleventh embodiment. This embodiment also provides the same effects as those in the above-described embodiments.

-Twelfth Embodiment-

Fig. 24 shows an arrangement of electrodes of a progressive method plasma display according to a twelfth embodiment of the present invention. In the above sixth to eleventh embodiments, the description has been made on the case in which the sustain electrodes and the scan electrodes constituting the display cells are alternately provided. More specifically, the scan electrodes to be scanned for application of an address selection voltage and the sustain electrodes to which the address selection voltage is not applied are alternately provided. In the twelfth embodiment, two adjacent scan electrodes  $Y_{n+1}$ ,  $Y_n$  and the like and two adjacent sustain electrodes  $X_n$ ,  $X_{n+1}$  and the like are alternately provided.



-Thirteenth Embodiment-

Fig. 25 is a cross-sectional view of an ALIS method plasma display according to a thirteenth embodiment of the present invention. This configuration is basically the same as that of the progressive method plasma display in Fig. 11. In the ALIS method, however, all of intervals between the electrodes  $X_{n-1}$ ,  $Y_{n-1}$ ,  $X_n$ ,  $Y_n$ ,  $X_{n+1}$ , and  $Y_{n+1}$  are the same with no light shield 203 provided. Gaps between the electrodes  $X_{n-1}$  and  $Y_{n-1}$ , between the electrodes  $X_n$  and  $Y_n$ , and between the electrodes  $X_{n+1}$  and  $Y_{n+1}$  are first slits respectively, and gaps between the electrodes  $Y_{n-1}$  and  $X_n$  and between the electrodes  $Y_n$  and  $X_{n+1}$  are second slits respectively. In the ALIS method, sustain discharges in the first slits are performed in a first frame FR in Fig. 36 as an odd field, and sustain discharges in the second slits are performed in a second frame FR subsequent thereto as an even field. These odd and even fields are repeatedly performed. Each of the electrodes can perform sustain discharges with respect to adjacent electrodes on both sides. The ALIS method has the number of display lines (rows) twice that of the progressive method, and thus enables high definition.

Figs. 26A and 26B are timing charts each showing a driving method during the sustain period  $T_s$  of the ALIS method plasma display according to this embodiment, in which the sixth embodiment (Fig. 12)

is applied to the ALIS method. Fig. 26A shows the voltage waveforms of sustain discharges in an odd field OF, and Fig. 26B shows the voltage waveforms of sustain discharges in an even field EF. The voltage waveforms in the odd field OF are the same as those in the sixth embodiment (Fig. 12). In the even field EF, in comparison with the odd field OF, the voltage to the sustain electrodes  $X_{n-1}$ ,  $X_{n+1}$ , and the like on the odd-numbered rows is exchanged with the voltage to the sustain electrodes  $X_n$ ,  $X_{n+2}$ , and the like on the even-numbered rows.

-Fourteenth Embodiment-

Figs. 27A and 27B are timing charts each showing a driving method during the sustain period  $T_s$  of an ALIS method plasma display according to a fourteenth embodiment of the present invention, in which the seventh embodiment (Fig. 17) is applied to the ALIS method. Fig. 27A shows the voltage waveforms of sustain discharges in an odd field OF, and Fig. 27B shows the voltage waveforms of sustain discharges in an even field EF. The voltage waveforms in the odd field OF are the same as those in the seventh embodiment (Fig. 17). In the even field EF, in comparison with the odd field OF, the voltage to the sustain electrodes  $X_{n-1}$ ,  $X_{n+1}$ , and the like on the odd-numbered rows is exchanged with the voltage to the sustain electrodes  $X_n$ ,  $X_{n+2}$ , and the like on the even-numbered rows.

-Fifteenth Embodiment-

Figs. 28A and 28B are timing charts each showing a driving method during the sustain period  $T_s$  of an ALIS method plasma display according to a fifteenth embodiment of the present invention, in which the eighth embodiment (Fig. 18) is applied to the ALIS method. Fig. 28A shows the voltage waveforms of sustain discharges in an odd field OF, and Fig. 28B shows the voltage waveforms of sustain discharges in an even field EF. The voltage waveforms in the odd field OF are the same as those in the eighth embodiment (Fig. 18). In the even field EF, in comparison with the odd field OF, the voltage to the sustain electrodes  $X_{n-1}$ ,  $X_{n+1}$ , and the like on the odd-numbered rows is exchanged with the voltage to the sustain electrodes  $X_n$ ,  $X_{n+2}$ , and the like on the even-numbered rows.

-Sixteenth Embodiment-

Figs. 29A and 29B are timing charts each showing a driving method during the sustain period  $T_s$  of an ALIS method plasma display according to a sixteenth embodiment of the present invention, in which the ninth embodiment (Fig. 21) is applied to the ALIS method. Fig. 29A shows the voltage waveforms of sustain discharges in an odd field OF, and Fig. 29B shows the voltage waveforms of sustain discharges in an even field EF. The voltage waveforms in the odd field OF are the same as those in the ninth

embodiment (Fig. 21). In the even field EF, in comparison with the odd field OF, the voltage to the sustain electrodes  $X_{n-1}$  and the like on the odd-numbered rows is exchanged with the voltage to the sustain electrodes  $X_n$  and the like on the even-numbered rows.

-Seventeenth Embodiment-

Figs. 30A and 30B are timing charts each showing a driving method during the sustain period  $T_s$  of an ALIS method plasma display according to a seventeenth embodiment of the present invention, in which the tenth embodiment (Fig. 22) is applied to the ALIS method. Fig. 30A shows the voltage waveforms of sustain discharges in an odd field OF, and Fig. 30B shows the voltage waveforms of sustain discharges in an even field EF. The voltage waveforms in the odd field OF are the same as those in the tenth embodiment (Fig. 22). In the even field EF, in comparison with the odd field OF, the voltage to the sustain electrodes  $X_{n-1}$  and the like on the odd-numbered rows is exchanged with the voltage to the sustain electrodes  $X_n$  and the like on the even-numbered rows.

-Eighteenth Embodiment-

Figs. 31A and 31B are timing charts each showing a driving method during the sustain period  $T_s$  of an ALIS method plasma display according to an eighteenth embodiment of the present invention, in which the

eleventh embodiment (Fig. 23) is applied to the ALIS method. Fig. 31A shows the voltage waveforms of sustain discharges in an odd field OF, and Fig. 31B shows the voltage waveforms of sustain discharges in an even field EF. The voltage waveforms in the odd field OF are the same as those in the eleventh embodiment (Fig. 23). In the even field EF, in comparison with the odd field OF, the voltage to the sustain electrodes  $X_{n-1}$  and the like on the odd-numbered rows is exchanged with the voltage to the sustain electrodes  $X_n$  and the like on the even-numbered rows.

In the ALIS method, as shown in Fig. 25, the intervals of the first slits and second slits are the same and thus likely to cause error display. According to the thirteenth to eighteenth embodiments, even by the ALIS method, each display cell can perform stable sustain discharges without receiving adverse effects from adjacent electrodes.

Note that while the description has been made, in the thirteenth to eighteenth embodiments, on the case in which the voltage to the sustain electrodes on the odd-numbered rows is exchanged with the voltage to the sustain electrodes on the even-numbered rows between the odd field and the even field, the voltages to the scan electrodes may be exchanged with each other in place of the sustain electrodes.

-Nineteenth Embodiment-

Fig. 32A shows the configuration of a sustain electrode sustain circuit 910 and a scan electrode sustain circuit 960 according to a nineteenth embodiment of the present invention. The sustain electrode sustain circuit 910, corresponding to the sustain electrode sustain circuits 103a and 103b in Fig. 1, is connected to a sustain electrode 951. The scan electrode sustain circuit 960, corresponding to the scan electrode sustain circuits 104a and 104b in Fig. 1, is connected to a scan electrode 952. A capacitor 950 is constituted of the sustain electrode 951, the scan electrode 952, and a dielectric therebetween. The sustain electrode sustain circuit 910 has a TERES (Technology of Reciprocal Sustainer) circuit 920 and a power recovery circuit 930.

First, the description will be made on the configuration of the TERES circuit 920. A diode 922 has an anode connected to a first potential (for example,  $V_{s1} = V_s/2[V]$ ) via a switch 921 and a cathode connected to a second potential (for example, the ground) lower than the first potential via a switch 923. A capacitor 924 has one end connected to the cathode of the diode 922 and the other end connected to the second potential via a switch 925. A diode 936 has an anode connected to the cathode of the diode 922 via a switch 935 and a cathode connected to the sustain electrode 951. A diode 937 has an anode connected to the sustain electrode 951

and a cathode connected to the aforementioned other end of the capacitor 924 via a switch 938.

Next, the description will be made on the operation of the TERES circuit 920 without the power recovery circuit 930. The following description is made on the case in which a sustain discharge voltage shown in Fig. 33A is applied to the sustain electrode  $X_n$ . The above-described anode voltage  $V_{s1}$  is, for example,  $V_s/2[V]$ , and the cathode voltage  $V_{s2}$  is, for example,  $-V_s/2[V]$ . At time  $t_1$ , the switches 921, 925, and 935 are closed, and the switches 923 and 938 are opened. Then, the potential of  $V_s/2$  is applied to the sustain electrode 951 via the switches 921 and 935. Besides, the electrode on the upper side (hereafter referred to as the upper end) in the drawing is connected to  $V_s/2$ , and the electrode on the lower side (hereafter referred to as the lower end) in the drawing is connected to the ground so that the capacitor 924 is charged. In this event, the charges on the capacitor 924 are discharged via the switch 935 and the diode 936 to the capacitor 950.

Subsequently, at time  $t_2$ , the switches 925 and 938 are closed, and the switches 923 and 935 are opened. Then, the ground potential is applied to the sustain electrode 951 via the switches 925 and 938.

Subsequently, at time  $t_3$ , the switches 923 and 938 are closed, and the switches 921, 925, and 935 are opened. Then, the capacitor 924 has the upper

end at the ground and the lower end at  $-V_s/2$ . The cathode potential of  $-V_s/2$  is applied to the sustain electrode 951 via the switch 938.

Subsequently, at time  $t_4$ , the switches 923 and 935 are closed, and the switches 921, 925, and 938 are opened. Then, the ground potential is applied to the sustain electrode 951 via the switches 923 and 935.

As described above, the use of the TERES circuit 920 enables generation of the anode potential  $V_{s1}$ , the cathode potential  $V_{s2}$ , and an intermediate potential  $(V_{s1} + V_{s2})/2$  with a simple circuit configuration.

Next, the description will be made on the configuration of the power recovery circuit 930. A capacitor 931 has a lower end connected to the lower end of the capacitor 924. A diode 933 has an anode connected to an upper end of the capacitor 931 via a switch 932 and a cathode connected to the anode of the diode 936 via a coil 934. A diode 940 has an anode connected to the cathode of the diode 937 via a coil 939 and a cathode connected to the upper end of the capacitor 931 via a switch 941.

Next, the description will be made on the operation of the power recovery circuit 930 with reference to Fig. 33B. First, at time  $t_1$ , the switches 921, 925, and 935 are closed, and the other switches are opened. Note that while the switch 935



is closed here, the switch 932 is closed before time  $t_1$  and thus may be kept closed also from time  $t_1$  to time  $t_2$ . Then, the potential of  $V_s/2$  is applied to the sustain electrode 951 from the power supply and the capacitor 924 via the switches 921 and 935. The capacitor 924 is charged to the potential of  $V_s/2$  from the power supply as well as discharges it to the capacitor 950 of the sustain electrode 951.

Subsequently, at time  $t_2$ , the switch 935 is opened, and the switch 941 is closed. Then, the charges on the sustain electrode 951 are supplied to the upper end of the capacitor 931 via the coil 939. The lower end of the capacitor 931 is connected to the second potential (GND) via the switch 925. Due to an LC resonance of the coil 939 and the capacitor (panel capacitance) 950, the capacitor 931 is charged so that power is recovered. This lowers the potential of the sustain electrode 951 to near  $V_s/4$ . Further, the diodes 940 and 937 remove the resonance, and the coil 939 can stabilize the potential of the sustain electrode 951 at near  $V_s/4$ .

Subsequently, at time  $t_3$ , the switch 938 is closed. Then, the potential of the sustain electrode 951 becomes the ground.

Subsequently, at time  $t_4$ , the switches 941 and 938 are opened, thereafter the switches 921 and 925 are opened, and the switch 923 is closed. Subsequently, the switch 941 is closed. The sustain

electrode 951 is connected to the ground via the diode 937, the coil 939, the diode 940, the switch 941, the capacitor 931, the capacitor 924, and the switch 923. Then, due to the LC resonance, the potential of the sustain electrode 951 lowers to near  $-V_s/4$ .

Subsequently, at time  $t_5$ , the switch 938 is closed. The potential of the sustain electrode 951 lowers to  $-V_s/2$ .

Subsequently, at time  $t_6$ , the switches 941 and 938 are opened, and the switch 932 is closed. Due to the LC resonance, the potential of the sustain electrode 951 lowers to near  $-V_s/4$ .

Subsequently, at time  $t_7$ , when the switch 935 is closed, the potential rises to the ground. Thereafter, the switches 932 and 935 are opened, the switch 923 is opened, the switches 921 and 925 are closed, and the switch 938 is closed.

Subsequently, at time  $t_8$ , the switch 938 is opened, and the switch 932 is closed. The potential of the sustain electrode 951 rises to near  $V_s/4$ . Thereafter, a cycle of the above-described time  $t_1$  to time  $t_8$  can be repeated.

The configuration of the scan electrode sustain circuit 960 is similar to that of the sustain electrode sustain circuit 910. The use of the power recovery circuit 930 can improve the energy efficiency to reduce the power consumption.

-Twentieth Embodiment-

Fig. 32B shows the configuration of a sustain electrode sustain circuit 910a according to a twentieth embodiment of the present invention. The description will be made on the point of the sustain electrode sustain circuit 910a differing from the circuit 910 in Fig. 32A. The sustain electrode sustain circuit 910a is made by omitting the switches 921, 923, and 925, the diode 922, and the capacitor 924 in Fig. 32A, connecting the switch 935 between the anode of the diode 936 and the power supply of  $V_s/2$ , and connecting the switch 938 between the cathode of the diode 937 and the power supply of  $-V_s/2$ .

Next, the description will be made on the operation of the sustain electrode sustain circuit 910a with reference to Fig. 33C. First, at time  $t_1$ , the switch 935 is closed, and the other switches are opened. Note that while the switch 935 is closed here, the switch 932 is closed before time  $t_1$  and thus may be kept closed also from time  $t_1$  to time  $t_2$ . The sustain electrode 951 is connected to the power supply of  $V_s/2$  and sustains the potential of  $V_s/2$ .

Subsequently, at time  $t_2$ , the switch 935 is opened, and the switch 941 is closed. The sustain electrode 951 is connected to the capacitor 931 via the switch 941, and lowers in potential to near  $-V_s/4$  due to an LC resonance.

Subsequently, at time  $t_3$ , the switch 938 is closed. The sustain electrode 951 is connected to the power supply of  $-V_s/2$  and sustains the potential of  $-V_s/2$ .

Subsequently, at time  $t_4$ , the switches 941 and 938 are opened, and the switch 932 is closed. The sustain electrode 951 is connected to the capacitor 931 via the switch 932 and lowers in potential to near  $V_s/4$  due to the LC resonance. Thereafter, a cycle of the above-described time  $t_1$  to time  $t_4$  can be repeated.

As described above, in the high image quality mode, sustain discharge pulses to all adjacent electrodes rise or fall at different timings as shown in Fig. 2 and so on. During performance of the sustain discharges between first and second display electrodes, the applied voltage to third electrodes adjacent to the first and second electrodes performing the sustain discharges and the polarity of wall charges formed on the third electrodes are controlled, thereby preventing the charges on the first and second electrodes from diffusing to the adjacent electrodes to eliminate error display. With an increase in definition of plasma displays, the distance between electrodes becomes shorter and likely to cause interference between adjacent display cells. The interference between them is suppressed,

whereby stable operation can be realized by increased margin of operating voltage.

Besides, in the low power mode and the high luminance mode, sustain discharge pulses to predetermined adjacent electrodes rise or fall in the same direction at the same time as shown in Fig. 3. In the low power mode, the plasma display device can perform a low power display when driven with the same number of sustain discharge pulses as that in the high image quality mode. In the high luminance mode, the plasma display device can perform a high luminance display when driven with the same power consumption as that in the high image quality mode, because the number of sustain discharge pulses increases.

The present embodiments are to be considered in all respects as illustrative and no restrictive, and all changes which come within the meaning and range of equivalency of the claims are therefore intended to be embraced therein. The invention may be embodied in other specific forms without departing from the spirit or essential characteristics thereof.

As has been described, it is possible to prevent changes on the X electrode and the Y electrode for performing a sustain discharge from diffusing to adjacent electrodes in the second sustain drive mode, thus making it possible to eliminate an error display and perform a high image quality display. In the

first sustain drive mode, the plasma display device can perform a low lower display when driven with the same number of discharge pulses as that in the second sustain drive mode, and can perform a high luminance display when driven with the same power consumption as that in the second sustain drive mode because the number of sustain discharge pulses increases.